

OPTICS

$$R_{10} \Rightarrow \frac{u_p}{u_r}$$

$$(M_T)_{\text{for lens}} \Rightarrow \left[\frac{f}{f+u} \right]$$

① deviation of two successive reflⁿ $\delta = 2\pi - 2\theta$

$$\text{② } v = \frac{uf}{u-f}$$

③ minimum size of mirror required

⑦ Axial magnification

④ field of view \rightarrow use Δ similarity $u = 2x$

$$M_{ax} = |M_{TA} \times M_{TB}| \rightarrow$$

④ effect of rotation of incident ray & mirror on reflected ray

$$M_{ax} = |M_T|^2 \rightarrow \text{short linear object}$$

i) incident ray: with same speed rotates reflected ray

ii) mirror: doubles the incident ray θ .

⑧ Relative motion in spherical mirror

$$V_{o/m} = (V_{I/m}) = V_I = V_{I/O}$$

$$m_T = \frac{f}{f-u}$$

$$\Rightarrow V_{I/m} = -(M_T)^2 \times V_{o/m}$$

⑨ Relative motion in plane mirror

$$\vec{V}_{o/m} = (V_{o/I})\hat{i} + (V_{o/II})\hat{j}$$

when mirror at rest.

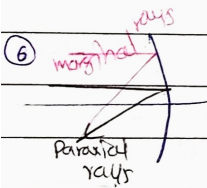
⑩ Snell's law

$$u \sin \theta = \text{const} \text{ or } \sin \theta = 1/u$$

$$\begin{matrix} \vec{V}_{o/m} & \rightarrow & \vec{V}_{I/m} & \rightarrow & \vec{V}_I & \rightarrow & \vec{V}_{I/O} \\ \text{(Rel)} & & \text{(SRT)} & & \text{(Rel)} & & \text{(SRT)} \end{matrix}$$

a) multiple medium

$$u_1 \sin \theta_1 = u_2 \sin \theta_2 = u_3 \sin \theta_3 = \dots$$



$$u_w = 4/3 \Rightarrow 1.33$$

$$u_g = 3/2 \Rightarrow 1.5$$

$$u_{air} = 1$$

⑪ dependence of focal length on angle of incidence

b) vector form of light $\hat{i} \times \hat{n} = u (\hat{r} \times \hat{n})$

$$f = \frac{R - R}{2 \cos i} \quad i = \text{large}$$

$$\lambda_{\text{med}} = \frac{\lambda_{\text{vacuum}}}{u_{\text{med}}} \quad \nu_{\text{med}} = \lambda_{\text{vacuum}} u_{\text{med}}$$

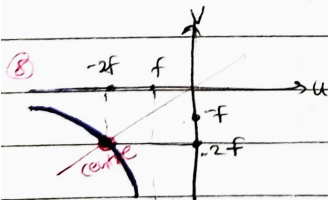
$$f = \frac{R}{2} \quad i = \text{small}$$

⑫ real & Apparent depth

a) when object is in denser med. & observer in rarer medium

$$\text{Apparent depth} = \frac{\text{Real depth}}{u}$$

$$\text{shifting} = h(1 - 1/u)$$



⑬ mirror formula $\frac{1}{f} = \frac{1}{v} + \frac{1}{u}$

b) object is in rarer medium and observer is in denser medium,

$$\text{App. ht} = u \times \text{Real depth}$$

$$\text{App. ht} = u \times \text{Real ht}$$

⑭ Transverse magnification

$$M_T = \frac{I}{O} = \frac{v}{u} \Rightarrow \frac{f}{f-u}$$

we for lens $v = \frac{uf}{u-f}$

(16) thickness of glass slab

$$t = u (v_1 + v_2)$$

$v_1 = \text{image dist.}$
 $v_2 = \text{image dist.}$

(15) Real & App. depth when Multiple med.

$$X_{\text{obj/observer}} = \mu_{\text{observer}} \left[\frac{x_1}{\mu_1} + \frac{x_2}{\mu_2} + \dots + \frac{x_n}{\mu_n} \right]$$

a) bird fish problem

$$X_{\text{fish/bird}} = \mu_B \left[\frac{y}{\mu_B} + \frac{x}{\mu_F} \right]$$

$$X_{\text{bird/fish}} = \mu_F \left[\frac{y}{\mu_B} + \frac{x}{\mu_F} \right]$$

Relative motion

$$V_{\text{fish/bird}} = \mu_B \left[\frac{v_B}{\mu_B} + \frac{v_F}{\mu_F} \right]$$

surface \rightarrow away = (+ve) like flux \rightarrow away (+ve)
towards surface = (-ve) density = (+ve)

(16) shifting of glass slab of image when kept b/w mirror & image

$$s = t \left[\frac{1 - \mu}{\mu} \right]$$

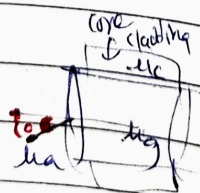
*** Total Internal Reflection ***

(1) $\sin i_c = \frac{\mu_e}{\mu_p} \Rightarrow D \mu_e$

- glass-air (i_c) $\Rightarrow 42^\circ$
- water-air (i_c) $\Rightarrow 48.5^\circ \Rightarrow 49^\circ$
- glass-water (i_c) $\Rightarrow 63^\circ$

(2) optical fiber

$$\sin i_c = \frac{\mu_g^2 - \mu_c^2}{\mu_a}$$



(8) Area of visible region

$$\text{Visible} = \frac{h}{\sqrt{\epsilon \mu_p^2 - 1}} \quad \text{Area} = \pi \epsilon l$$

$$\pi h^2 \epsilon \mu_p^2 - 1$$

Prism

(1) Snell's law

$$\mu_1 \sin i = \mu_2 \sin r_1$$

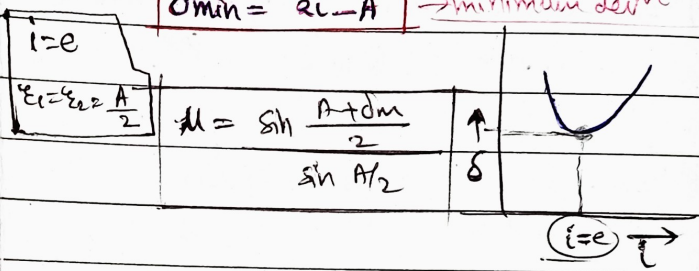
$$\mu_2 \sin r_1 = \mu_3 \sin e \quad \text{reflected deviation}$$

(2) deviation

$$\delta = 2(i - e)$$

$$\delta_{\text{net}} = i + e - A \quad \epsilon_1 + \epsilon_2 = A$$

$$\delta_{\text{min}} = r_1 - A \quad \rightarrow \text{minimum deviation}$$



$$\sin i = \mu \sin r_1$$

$$\sin i = \mu \sin A/2 \quad \rightarrow \text{minimum deviation}$$

\rightarrow under minimum deviation refracted ray is \parallel to base of prism \rightarrow isosceles triangle \rightarrow equivalent triangle

(3) condⁿ for TIR in prism

$$i_c < i_{\text{inc}} \text{ in prism}$$

$$\mu_c > \mu_{\text{prism}}$$

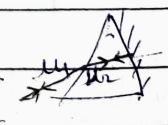
(A) Cauchy's theorem

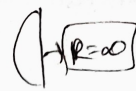
$$\mu = A + \frac{B}{\lambda^2}$$

- $\lambda_v < \dots < \lambda_r$
- $\mu_v > \dots > \mu_r$
- $(i_c)_v < \dots < (i_c)_r$

(5) silvering of prism

$$\mu_1 \sin i = \mu_2 \sin A$$





⑥ Thin prism (α = very small)

$$\delta = A(u-1) \quad \delta \theta \approx \alpha$$

→ Dispersion Mean Ray

$$\mu_y = \frac{\mu_v + \mu_r}{2} \quad \delta_y = A(\mu_y - 1)$$

⇒ Angular dispersion (θ)

$$\theta = A(\mu_v - \mu_r)$$

→ Dispersive power (ω)

$$\omega = \frac{\mu_v - \mu_r}{(\mu_y - 1)}$$

$$\frac{\omega}{\delta_y} = \text{Angular dispersion / dev of mean ray}$$

⑦ combination of prism of opposite action

- ① $\theta_{\text{net}} = \alpha_1 - \alpha_2$
 $\Rightarrow A_1(\mu_{v1} - 1) - A_2(\mu_{v2} - 1)$
- ② δ_{net}
 $\Rightarrow \delta_{y1} - \delta_{y2}$
 $\Rightarrow A_1(\mu_{y1} - 1) - A_2(\mu_{y2} - 1)$

a) Dispersion without devⁿ

i) No devⁿ: $\delta_y = \delta_{y1} - \delta_{y2} = 0$
 $\delta_{y1} = \delta_{y2}$

$$A_1(\mu_{y1} - 1) = A_2(\mu_{y2} - 1)$$

ii) Net dispersion $\theta_{\text{net}} = \alpha_1 - \alpha_2$

$$\Rightarrow A_1(\mu_{v1} - \mu_{r1}) - A_2(\mu_{v2} - \mu_{r2})$$

b) deviation without dispersion

i) No dispersion: $\theta_{\text{net}} = \alpha_1 - \alpha_2 \neq 0$

$$A_1(\mu_{v1} - \mu_{r1}) = A_2(\mu_{v2} - \mu_{r2})$$

ii) Net devⁿ:

$$\delta_{\text{net}} = \delta_{y1} - \delta_{y2}$$

$$A_1(\mu_{y1} - 1) - A_2(\mu_{y2} - 1)$$

⑧ I-O-S technique besides the lens's formula

(Applied for all condⁿ but it almost useful for more than two R.I having surfaces)

- (i) incident rays $\Rightarrow (-ve)$
- (ii) Refracted rays $\Rightarrow (+ve)$

⑨ Lens maker's formula

$$\frac{1}{f} = \left[\frac{\mu_2}{\mu_1} - 1 \right] \left[\frac{1}{R_1} - \frac{1}{R_2} \right]$$

a) equiconvex

$$F = R \quad 2(\mu_g - 1)$$

use for only Biconvex lens ($R_1 \neq R_2$)

b) equiconcave

$$F_{\text{ur}} = -R \quad 2(\mu_g - 1)$$

use for equiconcave ($R_1 = R_2$)

c) plano-convex

$$F_{\text{ur}} = R \quad (\mu_g - 1)$$

$$F_{\text{planoconvex}} = 2 F_{\text{equiconvex}}$$

⑩ comparison of focal length in air & liq.

$$\frac{F_{\text{air}}}{F_{\text{liq}}} = \frac{[\mu_g - 1]}{[\mu_l - 1]} \quad \left[\frac{\mu_g}{\mu_l} \right]$$

⑪ Two lenses separated by dist (d).

$$P_{\text{eq}} = P_1 + P_2 - d P_1 P_2$$

$$f_1 + f_2 = d \quad \text{then } P_{\text{eq}} = P_1 + P_2$$

$$f_{\text{eq}} = \frac{1}{\frac{1}{f_1} + \frac{1}{f_2}}$$

⑫ signing of plano-convex

a) signing of plane surface

$$f_{\text{eq}} = \frac{f_{\text{air}}}{2} \Rightarrow \frac{-f_{\text{liq}}}{2}$$

$$\left(\frac{-R}{2(\mu_g - 1)} \right)$$

$$\left(\frac{R}{2(\mu_l - 1)} \right)$$

$$\left(\frac{-R}{2(\mu_g - 1)} \right)$$

$$\Rightarrow \left(\frac{-R}{2(\mu_g)} \right)$$

$$\left(\frac{R}{(\mu_l - 1)} \right)$$

$u \sin \theta = \text{Numerical Aperture (radius of Aperture)}$
 $2u \sin \theta = \text{Aperture diameter}$

Optical Instruments

① Simple Microscope
 $\beta = \text{angle subtended by image}$
 $\alpha = \text{angle subtended by object}$

$$M_{\min} = \frac{D}{u_{\max}} \quad \left| \quad M = \frac{D}{u} = \frac{\beta}{\alpha} \right|$$

i) Eye under relaxed state or Normal vision

$$M_{\min} = \frac{D}{u_{\max}} = \frac{D}{E} \quad \left| \quad u_{\max} = F \right|$$

ii) Eye under strain / least distance vision

$$M_{\max} = 1 + \frac{D}{E} \quad \left| \quad u_{\min} = \frac{DF}{D+F} \right|$$

② Compound Microscope

i) $L = v_o + u_e$

ii) $m = -(m_o \times m_e) = \left(\frac{v_o}{u_o} \times \frac{D}{u_e} \right)$

a) eye in Relaxed state (Normal vision)

i) $L_{\max} = v_o + f_e$

ii) $M_{\min} = - \left[\frac{v_o}{u_o} \times \frac{D}{f_e} \right]$

b) eye under strain / least distinct vision

$$u_e = \frac{Df_e}{D+f_e}$$

① $L_{\min} = v_o + \frac{Df_e}{D+f_e}$

② $M_{\max} = - \left[\frac{v_o}{u_o} \times \left(1 + \frac{D}{f_e} \right) \right]$

$M_{\text{strain}} \Rightarrow \left(\frac{D}{D+f_e} \right)$ } valid for all optical instruments

③ Telescope (Astronomical)

$L = f_o + u_e^*$ $m = \frac{-f_o}{u_e}$ no matters in calculation

a) Normal adjustment

$L_{\max} = f_o + f_e$, $M_{\min} = \frac{f_o}{f_e}$

b) Eye under strain

$L_{\min} = f_o + \left(\frac{Df_e}{D+f_e} \right)$ $M_{\max} = \frac{f_o}{f_e} \left(1 + \frac{f_e}{D} \right)$

Resolving Power

Telescope R. Limit $\Rightarrow \frac{1.22 \lambda}{a} = \frac{1.22 \lambda}{24500 \theta}$

R. Power $\Rightarrow \frac{a}{1.22 \lambda}$

Microscope R. Limit $\Rightarrow \frac{1.22 \lambda}{24500 \theta}$

R. Power = $\frac{24500 \theta}{1.22 \lambda}$

$L = v_o + f_e$

$L = f_e$

optical density $\Rightarrow \frac{\text{speed of light in med. 1}}{\text{speed of light in med. 2}}$

Mach No. = $\frac{\text{speed of body}}{\text{speed of sound}}$

when v_o and u_o not given in question for compound microscope under normal adjustment

$$m = \left(\frac{L - (f_o + f_e)}{f_o} \right) \times \frac{D}{f_e}$$