

Wave Optics

(λ red) Red shift

Doppler's shift: $-c = \frac{v\lambda}{\Delta\lambda} = \frac{v f}{\Delta f}$

(λ blue) blue shift

Fresnel dist: $z_f = \frac{a^2}{\lambda}$

-ve sign means object goes distant

1) Interference

① $A_R = \sqrt{A_1^2 + A_2^2 + 2A_1A_2 \cos \Delta\phi}$

or $A_R = 2A_0 \cos \frac{\Delta\phi}{2}$

$A_{max} = A_1 + A_2$
$A_{min} = A_1 - A_2$

① new fringe width (w)

$w = \frac{\lambda D}{u d}$

② angular fringe width (β)

$\beta = \frac{\lambda}{u d}$

② $I_R = I_1 + I_2 + 2\sqrt{I_1 I_2} \cos \Delta\phi$ $A^2 \propto I$

or $I_R = 4I_0 \cos^2 \frac{\Delta\phi}{2}$ for incoherent sources

$I_R = \frac{I_0}{2}$

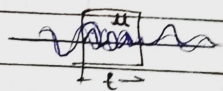
③ $I_{max} = 4I_0, I_{min} = 0$
 $A_{max} = 2A_0, A_{min} = 0$

* YDSE when white light is used

$n_1 \lambda_1 = n_2 \lambda_2$

$y_1 = \frac{n_1 \lambda_1 D}{d}$

No. of wave = $\frac{t u}{\lambda_{air}}$



optical path length = $u_{med} \times \text{thickness}$

2) YDSE

① $\Delta x = d \sin \theta = d y / D = n \lambda$ or $(2n-1) \frac{\lambda}{2}$

* Immo. of thin transparent sheet

$s = \frac{t(u_1)D}{d} = nD = x = \frac{n\lambda D}{d}$

② $y_{nth(max)} = \frac{n\lambda D}{d} = nD$

$y_{nth(min)} = \frac{(2n-1)\lambda D}{2d}$

① $y_{nth(max)} = \frac{n\lambda D}{d} + s$

$w = \lambda D / d$

no effect on angular width

3) Fringe width (w)

$w = \frac{\lambda D}{d}$

4) Angular fringe width

$\beta = \frac{w}{D} \Rightarrow \beta = \frac{\lambda}{d}$

$\sin \theta$ for absolute fringe

$\sin \theta_{(min)} = \frac{n\lambda}{d}$

$\sin \theta_{(max)} = \frac{(2n+1)\lambda}{2d}$

angular pos'n

angular width

$\sin \theta_1 = \frac{n\lambda}{d}$

$2\theta_1 = \frac{2n\lambda}{d}$

5) $\Delta\phi = \frac{2\pi}{\lambda} \cdot \Delta x$ $\Delta\phi = k \Delta x = \frac{2\pi}{\lambda} \Delta x$

linear pos'n

linear width of maxima

$y_1 = \frac{\lambda D}{d}$

$2y_1 = \frac{2\lambda D}{d}$

5) Fringe visibility / contrast

$V = \frac{I_{max} - I_{min}}{I_{max} + I_{min}}$

or $\frac{2\sqrt{n}}{n+1}$

$n = \frac{I_1}{I_2}$

Rayleigh's criteria

$\theta_{min} = \frac{1.22 \lambda}{d}$

linear width of max/min

$y_1 = \frac{2 \times (2n+1)\lambda}{2d}$

* YDSE in liquid

$\lambda_{med} = \lambda_{air}$
 u_{med}

$y_{nth(max)}(liq) = \frac{n\lambda D}{u d}$

Brewster law

$\tan \theta_p = \frac{\mu_2}{\mu_1}$
 $\sin i = \frac{\mu_2}{\mu_1}$



Polarization

$\frac{E_0}{B_0} = c$

$I = I_0$ - unpolarized
 $I_0 = I/2$ -> polarizer

$I_t = I_0 \cos^2 \theta$ -> Analyser (1) -> Brewster law of Malus

$I_{trans} = I_0 \cos^2 \theta_1 \cdot \cos^2 \theta_2 \cdot \cos^2 \theta_3 \dots \cos^2 \theta_n$

* YDSE from 3 slits etc $\cos^2 \theta$ केंद्रित क्षेत्र

Wave

① $v = \lambda/T \Rightarrow f \lambda = v/k$

② Angular wave no $k = 2\pi/\lambda$

③ Angular vel $\omega = 2\pi/T$

④ Transverse progressive wave eqⁿ

$y = A \sin(\omega t \mp kx + \phi_0)$

-ve sin \rightarrow (RHS)
+ve sin \rightarrow (LHS)

$y = A \cos(\omega t - kx + \phi_0)$

$a = -A \omega^2 \sin(\omega t \mp kx + \phi_0)$
angular wave no

⑤ speed of TPW on string

① $v = \sqrt{\frac{T}{\mu}}$
 $\mu = \text{mass of spring} / \text{linear mass length of string}$

$v = \sqrt{\frac{T}{\mu}} = \sqrt{\frac{T}{SA}} = \sqrt{\frac{T}{M/L}}$ ← for thin rope

② for thick rope

$\lambda \propto \sqrt{\text{Hanging mass}}$
 $v \propto f \lambda$
 $\therefore v \propto \sqrt{\text{Hanging mass (g)}}$

→ In thin rope velocity const $\sqrt{T/\mu}$
→ In thick rope accelⁿ const $(g/2)$

⑥ speed of sound wave

$v_{\text{sound}} = \sqrt{\frac{B_{ad}}{\rho}} = \sqrt{\frac{\gamma P}{\rho}} = \sqrt{\frac{\gamma RT}{M}}$

⑦ Intensity!

Power Area point source $\Rightarrow 4\pi r^2$

$A_{\text{max}} = A_1 + A_2$ $2A_0$
 $I_{\text{max}} = (I_1 + I_2)^2$ $4I_0$

⑧ Sound Level

$\beta = 10 \log_{10} \frac{I}{I_0}$ (dB) $I_0 = 10^{-12} \text{ W/m}^2$

$\beta_2 - \beta_1 = 10 \log \frac{I_2}{I_1}$

$\frac{A_{\text{max}}}{A_{\text{min}}} = \frac{A_1 + A_2}{A_1 - A_2}$

Interference

① $A_R = \sqrt{A_1^2 + A_2^2 + 2A_1A_2 \cos \Delta\phi}$

② $I_R = I_1 + I_2 + 2\sqrt{I_1I_2} \cos \Delta\phi$

③ $A_R = 2A_0 \cos \frac{\Delta\phi}{2}$ ④ $I_R = 4I_0 \cos^2 \frac{\Delta\phi}{2}$

constructive - I. $\Delta\phi = 2n\pi$
 $\Delta x = n\lambda$

destructive - I. $\Delta\phi = (2n-1)\pi$
 $\Delta x = (2n-1)(\lambda/2)$

④ $I_{\text{max}} = (I_1 + I_2)$
 $I_{\text{min}} = (I_1 - I_2)^2$

Beats

① Beat time $\Delta t = \frac{1}{|f_2 - f_1|}$

② Beat - freq $f_{\text{beat}} = |f_2 - f_1|$

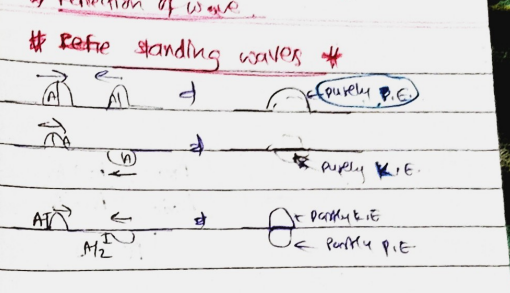
③ loading with wax of filing of Tuning fork

* Doppler's effect

$f_{\text{app}} = f \left(\frac{v - v_{\text{obs}}}{v - v_{\text{source}}} \right)$

$v_{\text{obs}} \rightarrow 0$ fine
 $v_{\text{obs}} \rightarrow -ve$

Transverse progressive wave eqⁿ $y = A \sin(\omega t + kx + \Delta\phi)$
standing wave eqⁿ $y = (2A \sin kx) \cos \omega t$



① standing wave eqⁿ

$y = (2A \sin kx) \cos \omega t$

Resultant amplitude or $(2A \cos kx) \sin \omega t$

② SWP on string

q. sonometer

stretched at both ends stretched at one end only

① $f = \frac{nV}{2L} = \frac{n}{2L} \sqrt{\frac{T}{\mu}}$ $f = \frac{(2n-1)V}{4L}$ $f = \frac{(2n-1)V}{4L}$

$n = \text{nth Harmonic}$ $(n-1)^{\text{th}}$ overtone
 $(n-1) = (n-1)^{\text{th}}$ overtone $(2n-1)^{\text{th}}$ Harmonic
 $(n=1)$ $f = \frac{V}{2L}$ fundamental freq $(2n-1) = (n=1)$ fundamental freq

$f_{\text{fundamental one end}} = \frac{1}{2} f_{\text{fundamental both end}}$

q. SWP on open organ pipe SWP on one end closed pipe

Resonance column

① $\lambda = 2(L_2 - L_1)$

② $v = f \lambda$

③ $4te = \lambda/4$ $4e = L_2 - 3L_1$
 $L_2e = 3\lambda/4$
 $L_2te = 5\lambda/4$

end correction

open pipe $f = \frac{n}{2L} \sqrt{\frac{\gamma RT}{M}}$